

An Audio Amplifier Power Supply Design

National Semiconductor
Application Note 1849
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Introduction

This application note provides design information for a power supply for use with National Semiconductor's newest offering of high-performance, ultra high-fidelity audio amplifier input stage ICs.

Analog audio circuit power supplies can have an audible effect in listening test and quantifiable effect in bench measurement results. Power supply designs that operate from the power mains are of three common types: Switch mode (SMPS), regulated, and unregulated power supplies.

Switch mode power supplies have become very popular, common, inexpensive, and readily available. SMPS are used extensively in computer hardware. They are well suited for such use providing good regulation with high efficiency in a small physical size. A drawback to SMPS is the switching nature of the design which creates EMI and RFI plus electrical noise on the supply rails. Small signal analog circuits are more susceptible to noise in the form of EMI or electrical noise on the supply lines. Certain classes of amplifiers, namely Class G and Class H, may be more easily realized with SMPS that are fast responding for full audio bandwidth signals. Using SMPS for audio circuits presents additional design challenges than when using a SMPS for non-audio circuits.

A regulated supply can be a simple linear regulator IC with the rectified voltage from the transformer as input and a handful of external components or any number of more complicated and often higher performance designs. There are the tradeoffs of complexity, cost, space, thermal design, reliability and protection with any regulated design. It is common for regulated supplies to be used for the analog small signal portions and other sensitive circuits for best performance. For an audio power amplifier, regulated supplies will need high bandwidth for good audio performance. The complexity and cost for such a power supply design may not be acceptable. Most linear regulator ICs do not have high bandwidth and are slow compared to audio signals which can result in reduced audio performance.

For simplicity, good performance, and reasonable cost, an unregulated supply is the most common for an audio power amplifier. An unregulated supply uses a transformer, a bridge rectifier, and various rail capacitors. A drawback to the unregulated supply is the voltage fluctuations with load and power mains fluctuations. A design should allow for a minimum 10% high line condition on the power mains. Unregulated supplies may have only a fuse in the power mains input to protect against excessive current unlike more sophisticated regulated designs. Additionally, the power supply voltage rails may have inline fuses to add some additional protection.

The circuit and solution presented in this application note has not been tested to any industry standards. It is the responsibility of the reader to perform standard industry testing to assure safety when using the solution in part or in whole in any form. National Semiconductor does not provide any guarantees, written or implied, about the safety of the solution.

Overview

This application note will cover the design of a $\pm 72V$ unregulated power supply designed specifically for the LME49810, LME49811 and LME49830 high-fidelity audio amplifier modules. The output power of the modules are approximately 220W to 250W into 8Ω and 350W to 400W into 4Ω . Complete documentation for the amplifier modules can be found in the documents listed below.

AN-1625 LME49810TB Ultra-High Fidelity, High-Power Amplifier Reference Design

AN-1850 LME49830TB Ultra-High Fidelity, High-Power Amplifier Reference Design

Although the power supply design is specific to the amplifier modules the concepts and circuit design may be used for any power supply purpose.

The power supply is an unregulated design with an option to allow connection to either 120V or 240V mains. The design uses toroidal transformers, a fully integrated bridge, and various rail capacitors for ripple voltage reduction, noise suppression, and to act as high current reservoirs. Additional circuitry to control inrush current on power up and power up/down Mute control are also included. A complete schematic, PCB views, and Bill of Materials are provided for the power supply design.

Schematic and Design

POWER SUPPLY

Figure 1 shows the complete schematic of the power supply design. The heart of the design is the basic power supply consisting of the transformers, the bridge, and various capacitors. Many of the capacitors used may not be commercially necessary or may have a minimal effect on performance. Because the design is not a commercial design where tight cost constraints must be taken into account, additional capacitors are freely used. For a commercial design, bench and listening test or some other test criteria is recommended to determine the exact number, size, and type of external components required. A short explanation of the purpose of each capacitor at the primary side of the transformers, around the bridge and on the supply rails follows. Some capacitors are doubled up on the PCB for flexibility or to achieve the desired total capacitance.

- C_1, C_2, C_4 are to protect against turn on/off spikes caused when the power switch changes positions. C_3 is not used and is redundant.
- C_{S1}, C_{S2} are low value, ceramic capacitors to filter higher frequency noise right at the DC output of the diode bridge.
- C_{S3}, C_{S4} are the large reservoir capacitors to supply large current demands and stabilize the supply rails to minimize low frequency fluctuations. These are very large value electrolytic capacitors. Two capacitors are used to achieve the desired $40,000\mu F$ capacitance per rail.
- C_{S5}, C_{S6} are high quality film capacitors to filter higher frequency noise. Two footprints are used on the PCB for flexibility.

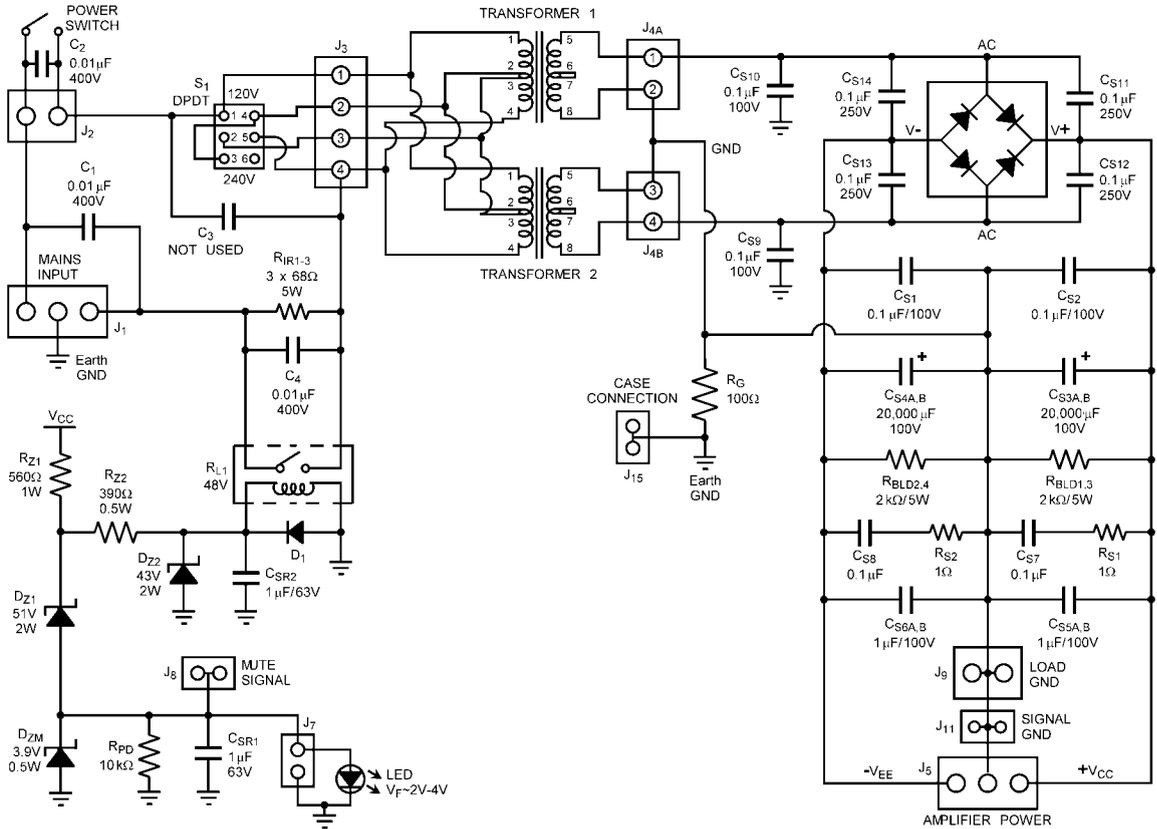
- C_{S7} , C_{S8} act in conjunction with R_{S1} and R_{S2} to decouple the large electrolytic capacitors and reduce impedance.
- C_{S9} , C_{S10} are low value, ceramic capacitors to filter higher frequency noise from the transformer secondary AC lines at the diode bridge.
- C_{S11} - C_{S14} are in parallel with the bridge diodes to reduce high frequency noise and ringing of the diode. An additional RC snubber in parallel with each diode of the rectifier will further reduce noise and ringing.

The values for the different capacitors were not chosen based on extensive bench work or research. The values were chosen based on general guidelines and commonly used values. Additional performance may be obtained through refinement

of the capacitor values. The equations and methods to determine optimal values are beyond the scope of this application note.

Additionally, the supply rails have bleeder resistors, R_{BL1} , R_{BL2} , to drain the large reservoir capacitors (C_{S3} , C_{S4}). Two footprints per rail were placed on the PCB to allow for lower power resistors to be used and a wide range of bleeder current. More sophistication can be added by including an additional DPDT relay and controls to only connect the bleeder resistors below a set voltage and remain unconnected during normal operation.

The fully integrated bridge has a peel & stick heat sink attached. (See Table 1) for robustness in use and higher ambient temperature conditions.



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FIGURE 1. Complete Power Supply Circuit

Additional Circuit

120V/240V SELECTION OPTION

For multi-country operation a switch is included to select between 120V or 240V input at the primary side of the transformers. The transformers are dual primary with the switch

allowing the option to put the primaries into series or parallel. The primary side of each transformer is connected in parallel for 120V operation with series connection used for 240V operation. The schematics below, Figures 2 and 3, show the different connections with the switch set for either 120V or 240V input from the power lines.

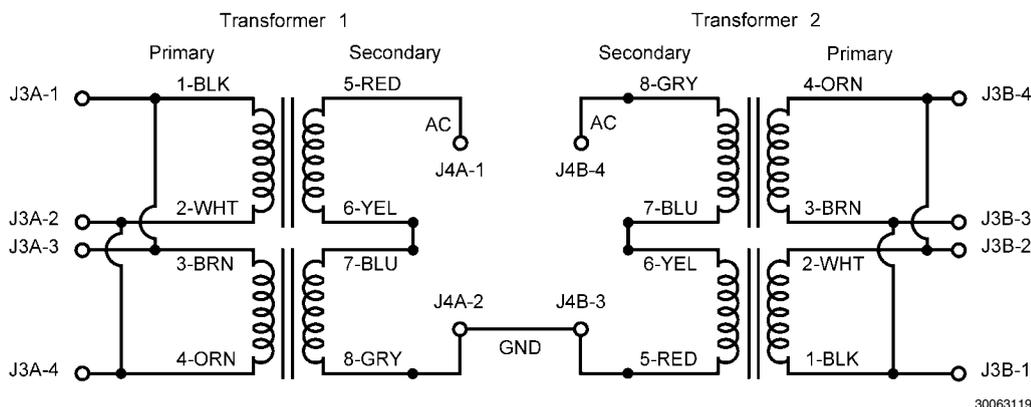


FIGURE 2. 120V Transformer Connections, Primaries in Parallel

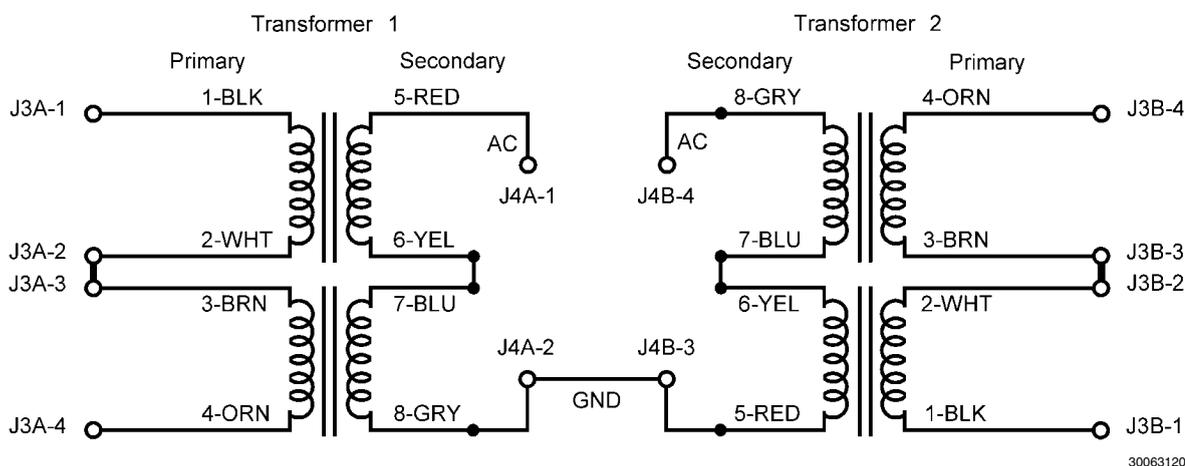


FIGURE 3. 120V Transformer Connections, Primaries in Series

across it. The LED's forward voltage (typically 2V ~ 4V) is used as the amplifier's Mute voltage. Setting the Mute resistor on the amplifier PCB module correctly allows the amplifier to go out of Mute mode once the LED's forward voltage is high enough to supply the needed Mute current. The LED is also used as an indicator, lighting when the amplifier is in Play mode. The values shown set the Mute voltage threshold to 57V on power up and 58V on power down. Because of component tolerances the threshold voltages will vary. At power down, the forward voltage of the LED will collapse quickly putting the amplifier into Mute mode well before the supplies are discharged for a quiet and relatively quick power off. Figures 7 and 8 show the Mute signal with supply voltage at power on and power off. There is additional delay from when the Mute signal reaches the Mute threshold (~1.80V for the amplifier PCB) and when the amplifier enters PLAY mode as a result of the mute delay capacitor on the amplifier PCB.

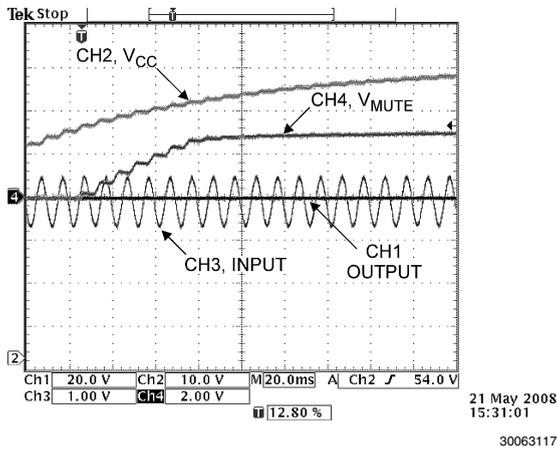


FIGURE 7. Mute at Power On

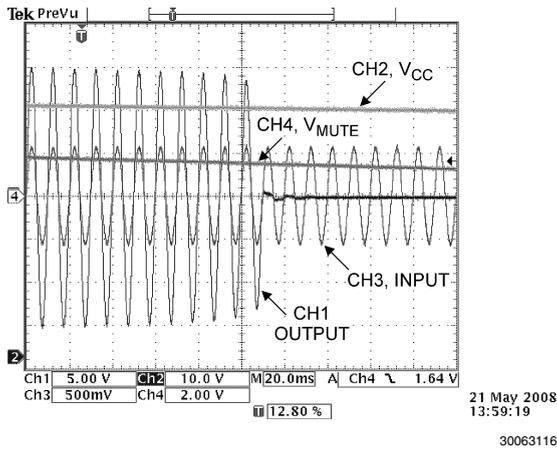


FIGURE 8. Mute at Power Off

The R_{ZM} Zener diode is for protection in the event of LED failure locking the Mute voltage so it will not exceed 4V. The amplifier PCB module's Mute resistor is sized for a maximum of 4V safely limiting Mute current. R_{PD} is needed so D_{Z1} will conduct and C_{SR1} is for a steady LED/Mute voltage.

A short coming of the simple Mute control circuit is the LED's brightness will vary under heavy amplifier load with the circuit values shown in Figure 6. Either the threshold of the Mute circuit can be lowered by changing the value of D_{Z1} for more consistent brightness in operation or a constant current circuit

may be used. Figure 9 shows a basic constant current (LED brightness) circuit with similar threshold voltages as the Mute control circuit.

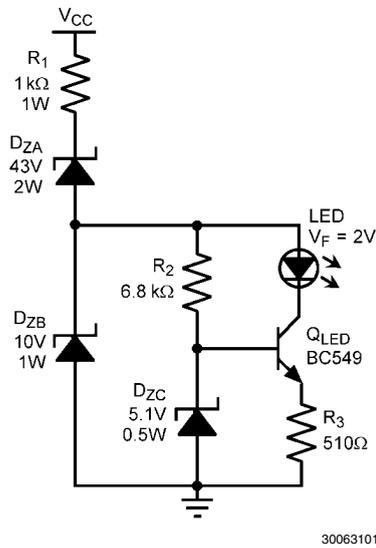
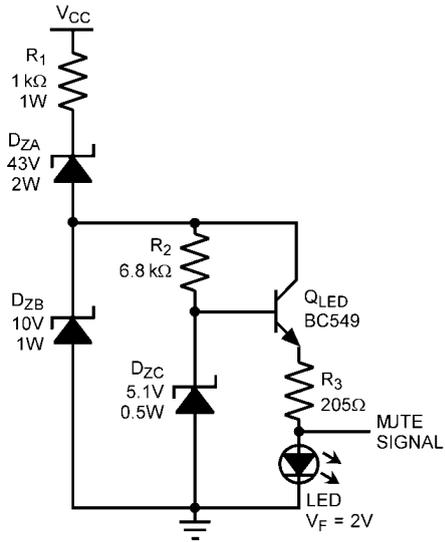


FIGURE 9. Constant Brightness LED Circuit

The LED will first begin to light when the positive supply rail voltage exceeds 45V. Once the positive rail reaches 60V the LED will have 6.5mA of current and only increase to 6.7mA at 80V with indiscernible change in brightness. Zener diode D_{ZA} sets the minimum threshold for first light of the LED. Combining the values of D_{ZA} , D_{ZB} , along with voltage drop across R_1 sets the voltage when the LED current reaches a constant value and constant brightness. R_3 and D_{ZC} set the LED current and R_2 is used to bias Q_{LED} and limit current through D_{ZC} . By using a 10V Zener diode (D_{ZB}) the power dissipation in Q_{LED} is kept very low so that a small transistor can be used without power dissipation concerns. The trade-off is that the D_{ZA} Zener diode is required to dissipation about 1W when the supply reaches 80V. Figure 9 does not give both constant LED current and the Mute signal control the same as Figure 6 although the Mute control could be taken at the emitter of Q_{LED} . An alternate circuit to combine both Figure 6 and 9 is shown in Figure 10.



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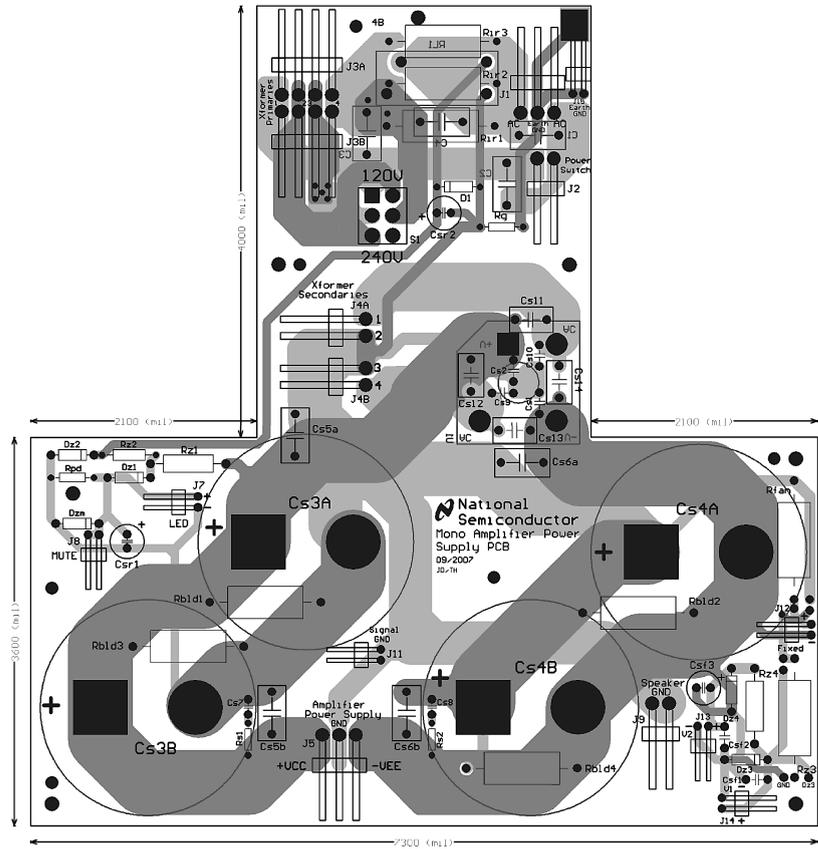
FIGURE 10. Constant Brightness LED and Mute Control Circuit

The circuit in Figure 10 will have the same threshold voltages as Figure 9 and similar Mute control thresholds as Figure 6 but can also be used to control the Mute signal to the audio amplifier module. For a reduced supply voltage window from LED first light to constant brightness, D_{ZA} should be increased while D_{ZB} is reduced. This will increase the LED first light threshold while reducing the additional voltage needed to reach the constant brightness threshold. The value of D_{ZC} may also be adjusted to achieve the designed circuit response.

Summary

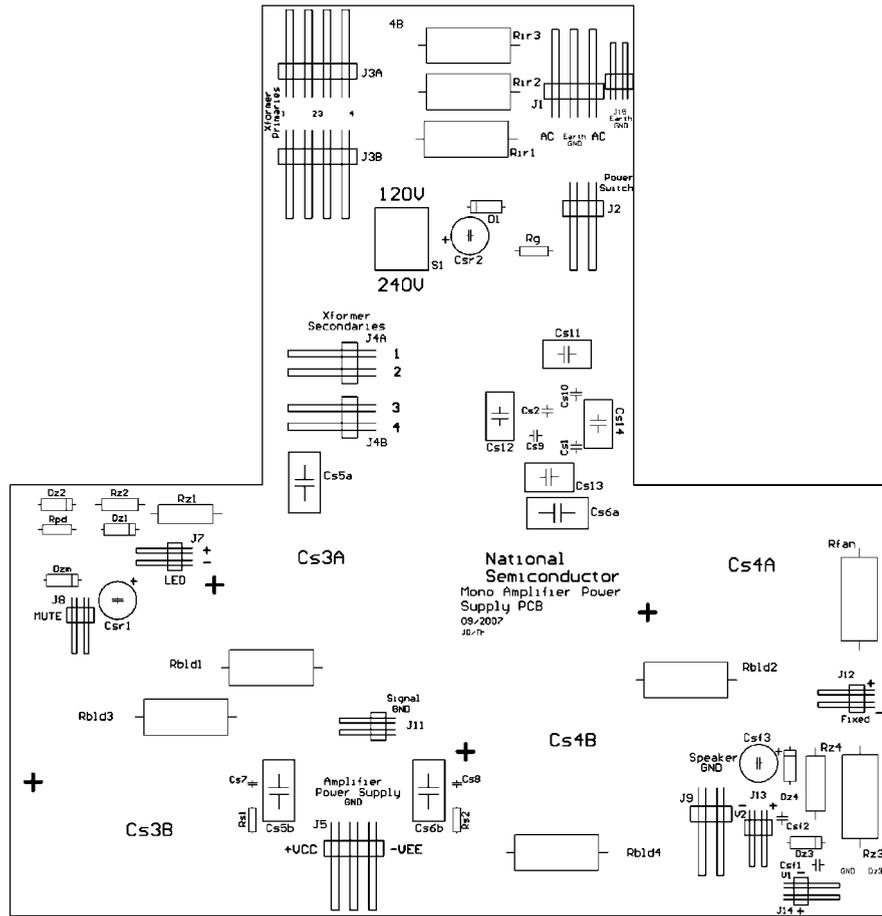
The unregulated power supply presented will give very good performance while powering an audio amplifier. While circuit modifications and additions can improve performance the solution presented has a relatively low part count and simplicity is maintained with all circuits. The power supply will provide a $\pm 70V$ to $\pm 73V$ supply under quiescent conditions with full load voltage dropping to $\pm 59V$ to $\pm 62V$.

Board Layer Views



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FIGURE 11. PCB Composite View From Top



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FIGURE 12. PCB Top Silkscreen View

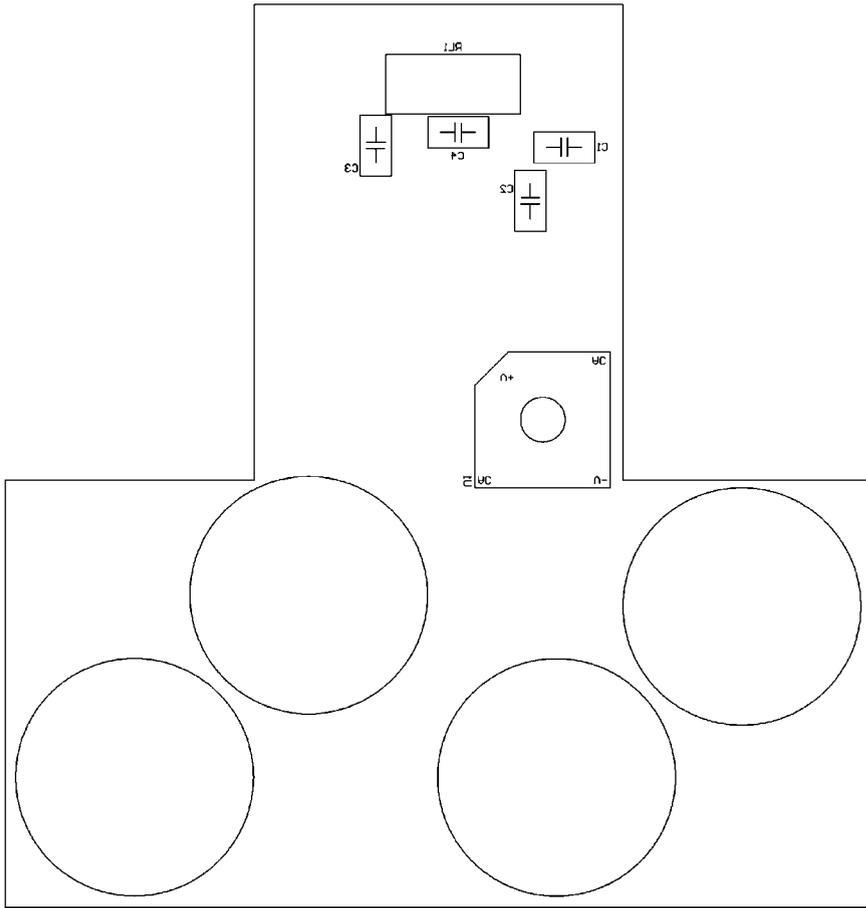
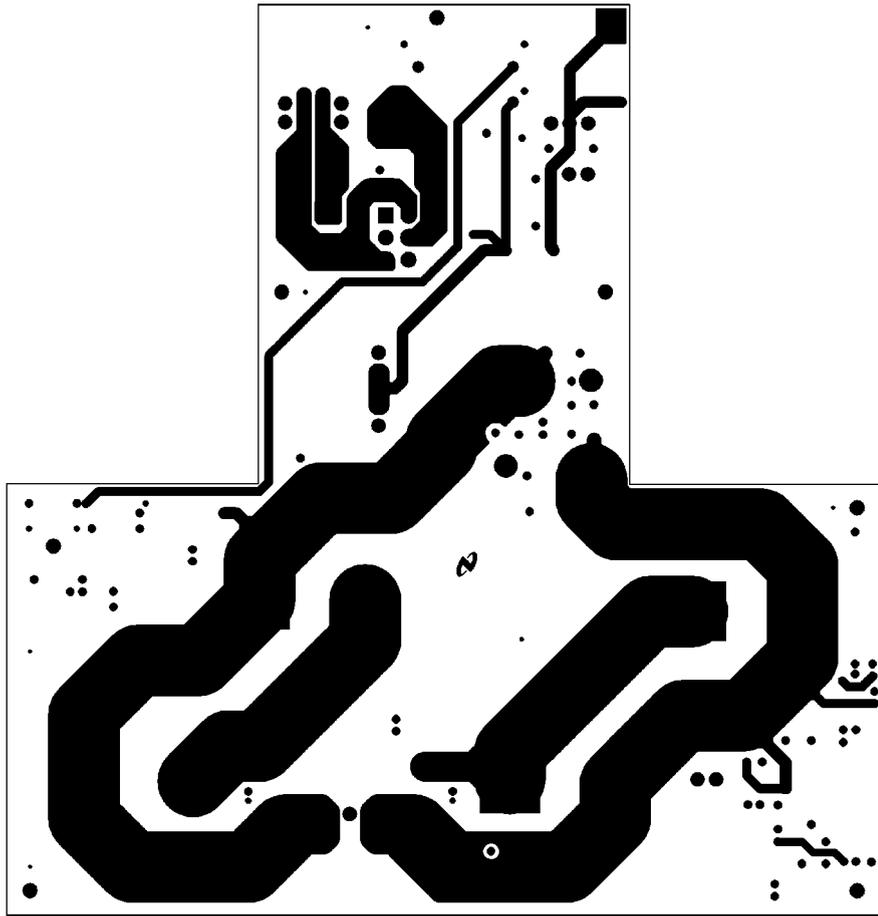
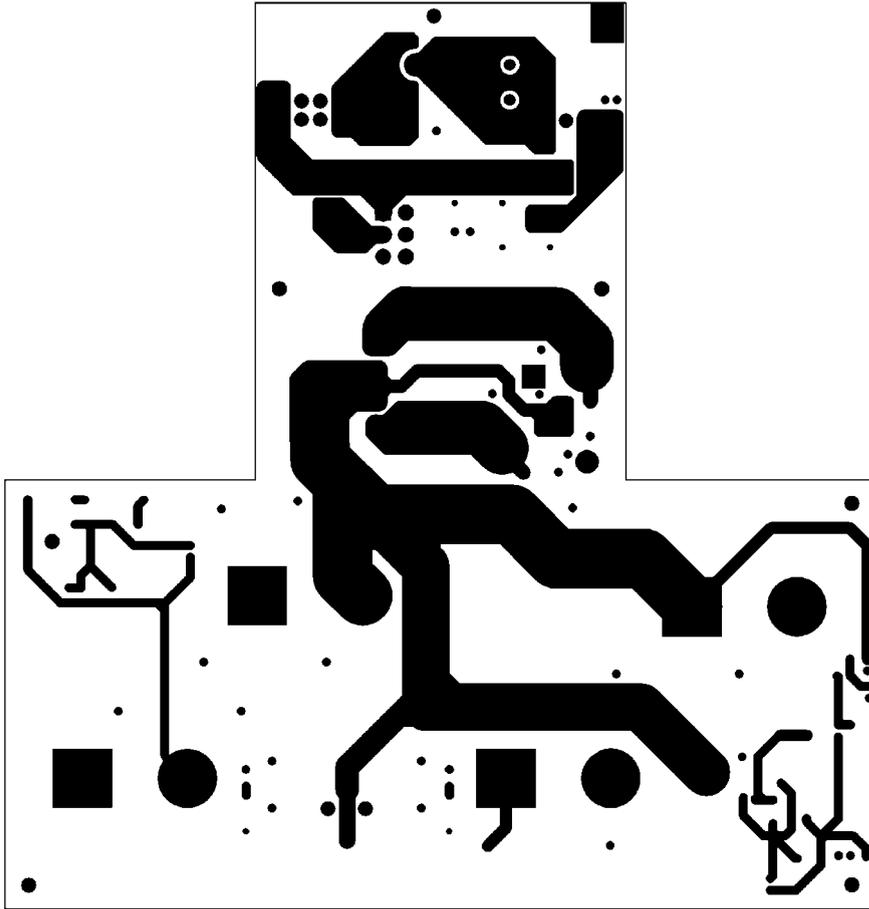


FIGURE 13. PCB Bottom Silkscreen View



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FIGURE 14. PCB Top Layer View



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FIGURE 15. PCB Bottom Layer View

Bill Of Materials

TABLE 1. Bill Of Materials

| Reference | Value | Tolerance | Description | Manufacturer | Part Number |
|--------------------------------|----------------|-----------|--|---------------------------------|------------------|
| C1, C2, C4 | 0.01 μ F | 10% | 400V, metalized polyester film, 7.5mm lead spacing | Panasonic | ECQ-E4103KF |
| C3 | | | Not Used | | |
| CS1, CS2, CS7, CS8, CS9, CS10, | 0.1 μ F | 10% | 100V ceramic, X7R type, 200mil lead spacing | AVX Corporation | SR211C104KAR |
| CS11, CS12, CS13, CS14 | 0.1 μ F | 10% | 250V, metalized polyester film, 7.5mm lead spacing | Panasonic | ECQ-E2104KF |
| CS3A, CS3B, CS4A, CS4B | 20,000 μ F | 20% | 100V electrolytic can | CDE Cornell Dubilier | DCMC203U100B C2B |
| CS5A, CS5B, CS6A, CS6B | 1 μ F | 10% | 100V, metalized polyester film, 10mm lead spacing | Panasonic | ECQ-E1105KF |
| CSR1, CSR2 | 1 μ F | 20% | 63V electrolytic radial, 2mm lead spacing | Panasonic | EEU-EB1J1R0S |
| D1 | 1A | | 400V diode, DO-41 | Vishay Semiconductor | 1N4004-E3/54 |
| DZ1 | 51V | 5% | 2W Zener diode, DO-41 | Microsemi Corporation | 2EZ51D5DO41 |
| DZ2 | 43V | 5% | 2W Zener diode, DO-41 | Microsemi Corporation | 2EZ43D5DO41 |
| DZM | 3.9V | 5% | 500mW Zener diode, DO-35 | Diodes Inc. | 1N5228B-T |
| RBLD1, RBLD2, RBLD3, RBLD4 | 2k Ω | 5% | 5W metal oxide | International Yageo Corporation | SQP500JB-2K0 |
| RFAN | 1.2k Ω | 5% | 5W metal oxide | International Yageo Corporation | SQP500JB-1K2 |
| RIR1, RIR2, RIR3 | 68 Ω | 1% | 5W wirewound silicone | Huntington Electric, Inc. | ALSR-5-68-1% |
| RS1, RS2 | 1 Ω | 5% | ¼ Watt carbon film | Panasonic | ERD-S2TJ1R0V |
| RG | 100 Ω | 1% | ¼ Watt metal film | International Yageo Corporation | MFR-25FBF-100 R |
| RZ1 | 560 Ω | 5% | 1 Watt metal oxide film | Panasonic | ERG-1SJ561 |
| RZ2 | 390 Ω | 5% | ½ Watt carbon film | Panasonic | ERD-S1TJ391V |
| RPD | 10k Ω | 5% | ¼ Watt carbon film | Panasonic | ERD-S2TJ103V |
| RL1 | 16A | | 48V, 400mW SPST, N.O., relay | Panasonic Electric Works | ALE15B48 |
| U1 | 35A | | 700V bridge rectifier | Fairchild Semiconductor | GBPC3510W |

| Reference | Value | Tolerance | Description | Manufacturer | Part Number |
|--------------------------------------|--|-----------|---|--------------------------------|---------------|
| S1 | 6A | | DPDT PCB mount, mini slide switch | C&K Components | 1201M2S1CQE2 |
| J1, J5 | | | 3 pin 156mil header, right angle, tin plating | Molex/Waldom Electronics Corp. | 26-60-5030 |
| J2, J9, J4A, J4B | | | 2 pin 156mil header, right angle, tin plating | Molex/Waldom Electronics Corp. | 26-60-5020 |
| J3A, J3B | | | 4 pin 156mil header, right angle, tin plating | Molex/Waldom Electronics Corp. | 26-60-5040 |
| J7, J8, J11, J12, J13, J14, J15 | | | 2 pin 100mil header, right angle, tin plating | Molex/Waldom Electronics Corp. | 22-05-3021 |
| Transformer1, Transformer2 | 24V, 300VA | | Dual primary, dual secondary, torrid transformer | Plitron Manufacturing Inc. | 77060201 |
| | $\theta_{CA} = 16.5^{\circ}\text{C/W}$ | | Peel & stick heat sink for bridge, 1.21" square, 0.55" tall | CTS Electronic Components, Inc | BDN12-5CB/A01 |
| RZ3, RZ4, DZ3, DZ4, CSF1, CSF2, CSF3 | | | Option unused circuits | | |

Revision History

| Rev | Date | Description |
|-----|----------|------------------|
| 1.0 | 06/03/08 | Initial release. |

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